Temperature dependence of the training effect in exchange coupled ferromagnetic bilayers

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Abstract: The temperature dependence of the training effect in an exchange coupled thin-film bilayer composed of a hard ferromagnetic pinning (CoPtCrB) layer in proximity of a soft ferromagnetic pinned (CoCr) layer is studied in a vast variety of systems including AF/FM systems. The EB TE is one of several commonly observed features associated with EB and biasing in HL/SL systems. It is defined as alteration of the EB bias field upon cycling the system through consecutive hysteresis loops and is quantified by \( \mu_0 H_{EB:B} \) vs \( n \), where \( n \) is the number of cycled loops. Training can be observed when the spin structure of the pinning layer is initially out of equilibrium and approaches the equilibrium spin configuration triggered via subsequent reversals of the pinned magnetization.

I. INTRODUCTION

Exchange bias (EB) is a coupling phenomenon which can be observed when an antiferromagnet and an adjacent ferromagnet share a common interface. Exchange coupling at the interface of antiferromagnetic (AF)/ferromagnetic (FM) thin films gives rise to a unidirectional anisotropy. Among the variety of effects related to the EB phenomenon the shift of the magnetic hysteresis loop along the magnetic field is the most prominent. This loop shift is quantified by the exchange bias field \( \mu_0 H_{EB} \).

The EB phenomenon was originally discovered more than 50 years ago by Meiklejohn and Bean. Since then EB has been observed in a vast variety of systems including AF/FM and FM/ferromagnetic thin-film heterostructures, AF/FM core shell nanoparticles, FM precipitates in AF and spin glass matrices, and spin valves; but details of its origin still remains elusive to date.3–7

Similar to exchange-spring magnets, AF coupled bilayers of soft and hard FM films show exchange-induced coupling phenomena analogous to conventional EB heterostructures.13–14 The FM hard layer (HL) pins the magnetically soft layer (SL) and shifts its hysteresis loops along the magnetic-field axis. The shift is quantified by the bias field \( \mu_0 H_B \). In the case of AF (FM) coupling, \( \mu_0 H_B \) is positive (negative) when the HL magnetization is set in a positive magnetization state and vice versa when the HL magnetization is negative. Antiferromagnetically coupled HL/SL bilayers are not only important in magnetic recording technology but can also be used as model systems to study EB and its related effects.15–17 HL/SL systems have several advantages over conventional AF/FM systems. For example, a FM pinning layer provides unique experimental access to the change in its magnetization state. In addition, the dependence of the bias field on the pinning layer magnetization can be directly measured by simple magnetometry.15,16 Moreover, AF materials are naturally inert to applied magnetic fields which limit the control of the AF domain state. Hence, isothermal tuning of the EB field and its training is very much limited to rare AF/FM systems. The situation is different when the pinning layer couples strongly to an applied magnetic field as it does in HL/SL heterostructures.

Training effect (TE) is one of several commonly observed features associated with EB and biasing in HL/SL systems. It is defined as alteration of the EB bias field upon cycling the system through consecutive hysteresis loops and is quantified by \( \mu_0 H_{EB:B} \) vs \( n \), where \( n \) is the number of cycled loops. Training can be observed when the spin structure of the pinning layer is initially out of equilibrium and approaches the equilibrium spin configuration triggered via subsequent reversals of the pinned magnetization.

Many investigations have been done on the EB TE which focus for instance on the influence of temperature, AF and FM film thicknesses, and dilution of the AF. The temperature dependence of the TE in conventional AF/FM systems is rather complex. Recent attempts to measure the correlation between aging of the interface magnetization in an AF pinning layer and the training of the EB field in AF/FM heterostructures faced serious difficulties because of the smallness of the excess magnetic moment in the AF pinning layer that gives rise to conventional EB. Theoretically the description of the \( T \) dependence of the TE in AF/FM systems is challenging due to the nontrivial relation between the AF order parameter and the magnetization. It is the AF interface magnetization which ultimately gives rise to the EB effect and its training behavior. Also, in these systems, proportionality between the moment at the interface and the AF bulk magnetic moment is a faintly motivated assumption. The latter is far more realistic in the case of a very thin FM pinning layer with a homogeneous spin structure along the normal of the film as demonstrated by the linearity of the effect. Recently it has been observed that small deviations from linearity can appear.

In all FM coupled systems training is initialized by partial demagnetization of the HL. Interestingly, and as an experi-
AF/FM exchange bias systems. Finally, we conclude in Sec. IV with an intuitive interpretation of our results.

In this article, we report a systematic study of the T dependence of bias field TE in all FM bilayers, in which a pinned SL is antiferromagnetically exchange coupled via a Ru intermediate layer with a pinning HL. We present a theory of the T dependence of TE which shows excellent agreement with our experimental data. The work presented in this paper is structured as follows. In Sec. II we describe the details of the sample, the experimental protocols, and the results of the measurements. In Sec. III we develop the theory, apply it to our experimental results, and bring it into context of our previous work including the training effect of AF/FM exchange bias systems.\cite{17,24,26,30,33} Finally we conclude in Sec. IV with an intuitive interpretation of our results.

II. EXPERIMENTAL DETAILS AND RESULTS

The SL of the sample under investigation is a CoCr film of 3 nm thickness. It is exchange coupled with a magnetically hard CoPtCrB pinning layer of 15 nm thickness via a Ru interlayer of thickness of 0.7 nm.\cite{17} Details of the sample fabrication can be found elsewhere.\cite{15,16} In the left frame of Fig. 1 the dotted line shows the overall magnetic hysteresis loops $m$ vs $\mu_0H$ (dotted red line). Solid black lines are typical minor (SL) loops after applying a set field of $H_{set}=-400\text{ mT}$. The horizontal line visualizes $m_r$ for the upper SL loop, the vertical line indicate the shift of the SL loop along the field axis relative to $\mu_0H=0$. The inset is the schematic of the sample. The right frame sketches the magnetic domain state of HL/SL heterostructure at different stages during the training cycle.

![Overall magnetic hysteresis loop](Figure1.png)

**FIG. 1.** (Color online) Overall magnetic hysteresis loop $m$ vs $\mu_0H$ (dotted red line). Solid black lines are typical minor (SL) loops after applying a set field of $H_{set}=-1/400\text{ mT}$. The horizontal line visualizes $m_r$ for the upper SL loop, the vertical line indicate the shift of the SL loop along the field axis relative to $\mu_0H=0$. The inset is the schematic of the sample. The right frame sketches the magnetic domain state of HL/SL heterostructure at different stages during the training cycle.
loops at horizontal lines which are isomagnetizations intercepting the we obtain groups of data sets labeled by which belong to the same isomagnetization line. By doing so initialized according to one of the isomagnetization lines temperatures within a group refer to various HL states ini-

...consistent with our training data, the SL magnetization rever-

...consequence the overall loop shows a small asymmetry and,

...The first $T=395$ K. The three broken lines show the set fields producing isomagnetic domain states after first and a large number set fields of the SL reveal a clear cycle-dependent relative shift along the field axis. The $n$ dependence is most pronounced for $T=395$ K. It can be quantified by the relative change in the bias field $\Delta H_B^\text{max}/H_B(n=1)=(H_B(n=15)−H_B(n=1))/H_B(n=1)$ which is 2.0% at $T=395$ K, 1.5% at $T=350$ K, 0.6% at $T=300$ K, and experimentally not resolvable at $T=200$ K for $M_{\text{ISO}}$ initialization. $\Delta H_B^\text{max}/H_B(n=1)$ is nonzero even below $T=300$ K but is rapidly dropping with decreasing temperature due to reduced thermal assistance of the triggered relaxation dynamics.

Figure 4 shows the detailed analysis, $\mu_B H_B$ vs $n$, of the SL training loops at $T=300$, 350, and 395 K for $M_{\text{ISO}}$ initialization. The $n$ dependence of $\mu_B H_B$ reflects the tendency of the HL to approach its quasiequilibrium of increased magnetization on subsequently cycled SL loops. The circles are the experimental data and the lines are the least-square fits of Eq. (5). Its theoretical background will be discussed later in the text. It is observed that the change in $\mu_B H_B$ is more pronounced for lower $n$ and it attains saturation for higher $n$.

It is the aim of the presented work to evidence that we achieve consistent description of all our experimental data with our theory of the TE. Particular emphasis lies on the understanding of the temperature dependence of the rate of change in $\mu_B H_B$ vs $n$ which up to now entered the theory as a free-fitting parameter only. Our Landau-type theory provides a functional form of the latter.

III. THEORY AND ANALYSIS OF EXPERIMENTAL RESULTS

The TE originates from the nonequilibrium nature of the spin structure in the pinning layer reflecting the gradual recovery of equilibrium triggered by consecutive hysteresis loops of the SL. Significant TE is achieved only when a set field drives the HL far out of saturation into a domain state. Consecutively cycled loops of the SL then trigger partial relaxation of the HL back toward saturation. Recently this mechanism has been experimentally evidenced. In the framework of this physical picture, the TE in all FM bilayers has been described theoretically by means of the discretized Landau-Khalatnikov (LK) equation,

$$S(n+1)−S(n) = \frac{1}{\tau} \frac{\partial \Delta F}{\delta S}.$$  

Here $S$ is the interface magnetization of the HL, $\tau$ and $\xi$ are the time and damping constants, respectively, $\Delta F$ is the
nonequilibrium free energy of the HL, $\Delta F$ quantifies the free energy increase when the HL magnetization $M$ deviates from its quasiequilibrium value $M_0$. The magnetization $M$ which plays the role of the order parameter allows us to express the free energy in terms of Landau-type series expansions. The overall HL magnetizations, $M$ and $S$, are proportional since $\partial M/\partial \varepsilon = 0$ is a reasonable assumption for all positions $(x, y)$ in the sample plane. The derivative $-\partial F/\partial S$ can be interpreted as a force that drives the HL domain state back toward the quasiequilibrium state of magnetization $M_0$. Hence, Eq. (1) is a discretized form of the equation of motion for $S$ in the regime of overcritical damping. Since $\mu_0H_B = c_1S$ and $M = c_2S$ we express the free energy in terms of $M$ and use later $\mu_0 H_B(n) = c_1 n M(n)$, with $c_{1,2} = \text{const.}$

Note that the description of dynamics via the Landau-Khalatnikov approach is unusual in magnetism but well established in ferroelectricity. Typically magnetization dynamics is described by the Landau-Lifshitz-Gilbert equation where an effective magnetic field creates a torque. This torque and a damping term together change the orientation of the magnetization vector. Here, however, the integral magnetization of the pinning layer is nonconserved since changes in the domain pattern are accompanied by changes in the overall magnetization. Relaxation of a nonconserved order parameter is dynamics of the model A type within the Hohenberg and Halperin classification schema and known to be described by the Landau-Khalatnikov equation. It has been explicitly shown for the simple case of a perfect ferromagnet with a regular array of up and down domains that the connection between the dynamic behavior and the domain structure is consistent with our Landau-Khalatnikov approach leading to Eq. (1). Note that the LLG approach when embedded in a micromagnetic simulation which divides a sample into homogeneously magnetized interacting finite elements or grains that is by all means capable of describing domain effects and is able to fully explain nonuniform magnetization reversal and realistic hysteresis loops. Our aim here is, however, a simple analytic approach that catches the essentials and allows for intuitive interpretation. For this purpose our integral view on the overall magnetization of the pinning layer with the help of the Landau-Khalatnikov approach is useful.

In our recent paper we derived the functional form $\mu_0 H_B = \mu_0 H_B(n)$ from Eq. (1) using the Landau-type free-energy expansion,

$$ F = F_0 + \frac{1}{2} \frac{\partial^2 F}{\partial M^2} \bigg|_{M=M^c} (M-M^c)^2, $$

in the vicinity of the quasiequilibrium magnetization, $M^c$, attained by the HL after a large number of SL hysteresis loops. A straightforward result using Eqs. (1) and (2) and the proportionality above is the implicit sequence,

$$ H_B(n+1) = (K+1)H_B(n) - KH^c_B, $$

where

![Figure 3](cid1)
which hitherto entered the theory as a fitting parameter only. We use Eq. (5) to obtain \( K \) values for all of our training data \( \mu_0 H_B vs n \) such as those shown exemplarily in Fig. 4. Least-squares fits of the function \( K(T) \) to these \( K \) values will evidence the consistency of the theory. Subsequently we outline the derivation of the function \( K(T) \) from Eq. (4).

In order to obtain the temperature dependence of \( \frac{\partial^2 F}{\partial M^2} \bigg|_{M=M_s} \), which contains the temperature dependence of \( K \) we compare Eq. (2) with the Landau expansion,

\[
F = F_0 + \frac{1}{2} a M^2 + \frac{1}{4} b M^4 - H M,
\]

in the vicinity of \( M=0 \), where \( a=a_0(T-T_C) \), \( T_C \) is the Curie temperature of the HL and \( a_0, b>0 \) are the constants. From Eq. (6) we obtain,

\[
\frac{\partial^2 F}{\partial M^2} \bigg|_{M=M_s} = a + 3b M_e^2
\]

where \( M_e \) is the solution of \( a M_e + b M_e^3 - H = 0 \) derived from \( \frac{\partial^2 F}{\partial M^2} \bigg|_{M=M_s} = 0 \). Since the magnetic fields applied during the training cycles are small in comparison to the HL coercive fields the Zeeman term in Eq. (6) is negligible and the equilibrium magnetization \( M_e \) can be expressed by the simple Landau expression \( M_e = \sqrt{-a/b} \) allowing us to simplify expression (7) which then reads \( \frac{\partial^2 F}{\partial M^2} \bigg|_{M=M_s} = 2b M_e^2 = 2a_0(T_C - T) \).

Substituting the latter expression into Eq. (4) we obtain,

\[
K = -T \frac{\partial^2 F}{\partial \xi^2} \bigg|_{M=M_s} < 0.
\]

Note that the decreasing accuracy of the simple Landau expression away from \( T_C \) is compensated to a large extent by the strong temperature dependence of the damping constant, \( \xi \), resulting in \( K(T\rightarrow0) \rightarrow 0 \) independent of the specific functional form of \( M_e(T) \). It can be shown that a mean-field solution for \( M_s(T) \) yields very similar results for \( K vs T \) while the advantage of a simple analytic form of the results is lost, however.

The damping constant is known to be temperature dependent in other ferroic systems such as organic thin-film ferroelectrics having the functional form,

\[
\xi \propto |T| \exp\left(\frac{2U}{kT}\right),
\]

with \( U \) being an energy barrier. The latter has the microscopic interpretation of a dipole/spin-flip energy. Using mean-field arguments this energy is given by \( U=(\zeta(\xi)\bar{s})^2 \), where \( \zeta \) is the number of nearest neighbors, \( J \) is the exchange energy, \( \bar{s} \) is the spin quantum number, and \( \langle \cdots \rangle \) denotes an average over the distribution of local configurations in the pinning layer alloy CoPtCrB. In mean-field approximation \( U \) is related to \( T_C \) via \( U=3s^2 k_B T_C [s(s+1)] \). In order to estimate an effective value of \( s \) for the alloy CoPtCrB we recall the Slater-Pauling curve and in particular the strong deviations from the latter for Co-alloys involving elements which are two atomic numbers or more apart such as Co-Cr for instance. Taking the strong suppression of the atomic magnetic moment in Co-alloys into account we use \( s=1/2 \) to
obtain $U = k_B T_C$. Using this result for the energy barrier and substituting Eq. (9) into Eq. (8) we obtain

$$K = -\frac{P}{N} e^{2T_C/T}(T_C - T),$$

where $P > 0$ is a free parameter.

The Curie temperature, $T_C$, of the HL enters Eq. (10) and, therefore, makes it preferable to have independent experimental access to its value. We estimate $T_C$ experimentally from the temperature dependence of the HL coercivity $\mu_0 H_C^\text{ISO}$ vs $T$ through extrapolation of the data to the intercept with the temperature axis. The left axis of Fig. 5 shows the coercivity data $\mu_0 H_C^\text{ISO}$ vs $T$ of the HL. The latter are obtained from the overall hysteresis loops displayed in Fig. 2. Note, however, that the apparent HL coercivity $H_C^\text{ISO}$, circles, and from a coupling-induced HL loop broadening, $H_C^\text{broad}$ itself is obtained from the overall loops after subtracting the SL magnetization. Correcting with respect to the coupling-induced broadening is a small but somewhat involved effect. The SL/HL coupling at $H_C$ of the SL is given by the bias field created by the fully saturated SL. Thus the bias coming from the SL and affecting the HL coercivity has to be related to the bias onto the SL that a fully magnetized HL generates $H_C^\text{max}$. Quantitatively the effect on the HL depends on the ratio of the SL/HL magnetizations and hence on the weighting factor $m_{SL}/m_{HL}$. The SL coupling contribution has to be subtracted to get the genuine HL coercivity. This correction is done by using $H_C = H_C^\text{ISO} - [H_B^\text{max} m_{SL}/m_{HL}]$. The hexagons in Fig. 5 are experimental $\mu_0 H_C^\text{ISO}$ vs $T$ data. The corresponding dotted line is the best linear fit. Extrapolation down to $\mu_0 H_C^\text{ISO}=0$ yields the HL Curie temperature $T_C = 583.5$ K. The linear extrapolation is the best we can do in the absence of a rigorous theory for $\mu_0 H_C^\text{ISO}$ vs $T$. In fact the simple Landau expression $a M_0 + b M_0^2 - H = 0$ predicts the nonlinear behavior $H_b = \sqrt{[-b a_0/(T - T_C)]} b$, which approaches the $T$ axis slower than the linear extrapolation implying a higher value of $T_C$. However, the intrinsic coercivity considered in the latter expression is never relevant in real ferromagnets. In addition $T_C = 583.5$ K obtained from the linear extrapolation is strongly supported by the fits of $\mu_0 H_C^\text{ISO}$ vs $T$ discussed in the next paragraph.

The right axis of Fig. 5 shows the equilibrium bias fields $\mu_0 H_B^\text{ISO}$ vs $T$ for the initializations $M_{\text{ISO1}}$ (squares), $M_{\text{ISO2}}$ (circles), and $M_{\text{ISO3}}$ (triangles). The lines represent single parameter fits of the function

$$\mu_0 H_B^\text{ISO}(T) = \mu_0 H_B^\text{ISO}(T = 0) \sqrt{T_C - T / T_C},$$

yielding $\mu_0 H_B^\text{ISO}(T = 0) = 99.73 \pm 0.97$, $96.93 \pm 0.82$, and $92.01 \pm 0.17$ mT for $M_{\text{ISO1}}$, $M_{\text{ISO2}}$, and $M_{\text{ISO3}}$, respectively. Note that the successful fit of Eq. (11) reconfirms the applicability of the simple Landau expression for the temperature dependence of the HL magnetization which leads to Eq. (8).

Finally Fig. 6 shows all $K$ vs $T$ data obtained from least-square fits of Eq. (5) to the experimental $\mu_0 H_B^\text{ISO}$ vs $n$ data (see lines for fits and circles for typical training data in Fig. 4). The experimental $K$ data in Fig. 6 originate from training initializations $M_{\text{ISO1}}$ (squares), $M_{\text{ISO2}}$ (circles), and $M_{\text{ISO3}}$ (triangles). Lines represent the results of a best fits of Eq. (10) to the respective data set where $P$ is the single free fitting with $P = 0.626 \pm 0.009$, $0.570 \pm 0.023$, and $0.572 \pm 0.0396 K^{-1/2}$ for $M_{\text{ISO1}}$, $M_{\text{ISO2}}$, and $M_{\text{ISO3}}$, respectively. As a typical example we show error bars for the $M_{\text{ISO1}}$
data. Next we briefly describe how these error bars are obtained.

While the $K$ values shown in Fig. 6 are determined from best fits of Eq. (5) to respective training data, an alternative determination of optimized $K$ values is obtained from the expression

$$K = \frac{\sum_{n=1}^{N-1} [H_B(n) - H_B^e][H_B(n+1) - H_B(n)]}{\sum_{n=1}^{N-1} [H_B(n) - H_B^e]^2}. \quad (12)$$

Here the $H_B^e$ is an input obtained from the fit of Eq. (5). Equation (12) is derived from a least-squares condition using Eq. (3). Expression (12) is used to calculate the standard deviation $S_K$ of $K$ from Gauss’ law of error propagation which reads as

$$S_K = \sqrt{\sum_{n=2}^{N} \left( \frac{\partial K}{\partial H_B(n)} \Delta H_B(n) \right)^2}, \quad (13)$$

where $\Delta H_B(n)$ is the error in the bias field of the $n$th training loop. The derivatives entering $S_K$ are calculated from Eq. (12) and read as

$$\frac{\partial K}{\partial H_B(n)} = \frac{[H_B(n-1) + H_B(n+1) - 2H_B(n)]}{\sum_{n=1}^{N-1} [H_B(n) - H_B^e]^2} - 2K \frac{\sum_{n=1}^{N-1} [H_B(n) - H_B^e]^2}{\sum_{n=1}^{N-1} [H_B(n) - H_B^e]^2}. \quad (14)$$

With $\Delta \mu H_B(n) = 0.1$ mT $\forall n$ it is straightforward to numerically determine $S_K$. The results of this analysis are shown for one example ($M_{ISO1}$) in Fig. 6 as error bars. Note that the magnitude of the error bars increases with decreasing temperature. When applying the same analysis to the $T = 200$ K data set where $\mu_0 H_B^e - H_B(1) = 0.1$ mT is extremely small $S_K = 0.3$ in turn becomes even significantly larger than the theoretically expected value of $[K] = 0.05$. Note that this increase in the error bar takes place despite the fact that the absolute accuracy of the bias fields remains $\Delta \mu_0 H_B(n) = 0.1$ mT [see Fig. 3(d)]. Hence it is obvious that any attempt to determine $K$ values at low temperatures where $\Delta H_B = H_B^e - H_B(1) \rightarrow 0$ will become experimentally virtually impossible.

The inset of Fig. 6 provides an intuitive understanding of the role of $K$ for the characteristics of the TE. A family of curves is displayed where $K$ is varied within the range of $-1 \leq K \leq 0$. This interval defines the range of convergence for the geometrical series involved in the transformation of the implicit sequence (3) into the explicit Eq. (5). The value of $K$ changes from 0 to $-1$ along the direction of displayed arrow. Inspection of Eq. (3) shows that $K=0$ yields $H_B(n + 1) = H_B(n)$ which means no training at all. Note that this does not imply that the bias field has to be zero. Similarly $\Delta H_B = H_B^e - H_B(1) \rightarrow 0$ does not necessarily imply $K \rightarrow 0$. $K = -1$ in turn yields $H_B(n+1) = H_B^e$ $\forall n \geq 1$ which means a step-like change in the bias field between the first two points and zero training for $n > 2$. Intuitively $K(T \geq T_C) = 0$ has to be fulfilled because $H_B(n+1) = H_B^e = 0 \forall n \geq 1$ at $T = T_C$ reflecting the absence of biasing and, hence, training. Similarly $K(T=0) = 0$ holds. Here, however, $K(T=0) = 0$ reflects the nontrivial situation where a nonzero-bias field can be accompanied by zero TE. Instead of zero-bias field associated with zero pinning layer magnetization a nonzero pinning layer magnetization can be frozen in at $T=0$. Domain walls are pinned and the absence of thermal activation keeps the pinning layer in the initial domain state. In the framework of Eq. (3) this freezing behavior is reflected by a diverging damping constant [see Eq. (9)] which give rise to $K=0$. In addition the $K=0$ state at $T=0$ is approached with $dK/dT \mid_{T=0} = 0$ similarly to the asymptotic behavior of equilibrium thermodynamic properties obeying the third law of thermodynamics.

It is hard to imagine any arbitrary single parameter fitting function which is consistent with the constraints $K(T=0) = 0$, $dK/dT \mid_{T=0} = 0$, and $K(T=T_C) = 0$ providing the quality of the fits as shown in Fig. 6. Moreover, the fitting parameters of Eqs. (10) and (11) reflect the ratio $P_{ISO1}/P_{ISO2} = 1.10$ $\approx [H_B^e(T=0,ISO1)/H_B^e(T=0,ISO2)]^2 = 1.06$ as expected from Eqs. (4) and (10) and the proportionality between $H_B^e$ and $M_c$.

IV. CONCLUSIONS

We have shown that bilayers of antiferromagnetically coupled hard and soft ferromagnetic thin films have prototypical properties providing fundamental understanding of exchange bias and its training effect. We demonstrated that in far reaching analogy to antiferromagnetic/ferromagnetic exchange bias heterolayers quantitative understanding of the temperature dependence of the training effect is achieved. Large training effects reflected by the parameter $-1 < K < 0$ require thermal activation allowing for triggered changes in the domain structure of the pinning layer but at the same time sufficient thermal stability of the pinning layer magnetization. This competition between thermal activation and stability creates maximum training effects at $T=T_C(\sqrt{41} - 5)/2$. The successful modeling of the temperature dependence of the training effect in our all FM bilayer system confirms the consistent description of training behavior in the discretized Landau-Khalatnikov approach.

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64 V. Stephanovich (private communication).